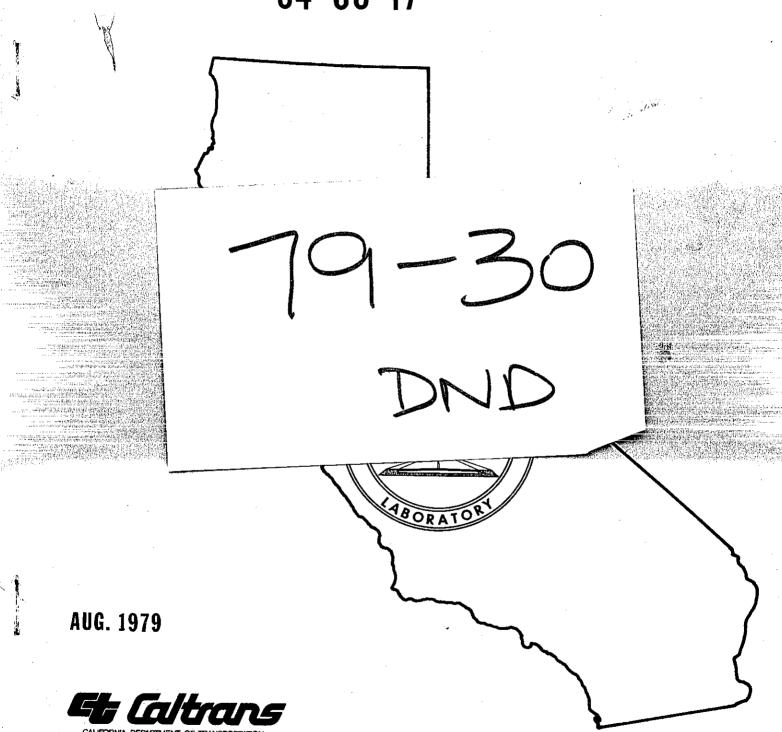
Richmond Semi-Depressed Section 04-CC-17



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STATE OF CALIFORNIA DEPARTMENT OF TRANSPORTATION DIVISION OF CONSTRUCTION OFFICE OF TRANSPORTATION LABORATORY

04-CC-17, PM 1.3 to 3.9 47th St. to 6th St. 04209-108701 Lab Auth 652907 August 1979

Mr. T. R. Lammers - 04 District Director of Transportation

Attention: Mr. D. T. Cassinelli

District Materials Engineer

Gentlemen:

Submitted for your consideration:

SUPPLEMENT TO THE
REPORT
OF
GROUND WATER INVESTIGATION
FOR THE
PROPOSED

RICHMOND SEMI-DEPRESSED SECTION
04-CC-17
(GROUND WATER QUALITY STUDY)

Very truly yours,

NEAL ANDERSEN Chief, Office of Transportation Laboratory

Raymond A. Forsyth

Chief Soil Mechanics and B

Chief, Soil Mechanics and Pavement Branch

SBPJ:db Attachment Distribution I and the second of the second

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INTRODUCTION

This supplementary report has been prepared to complete the ground water quality study started as part of the ground water investigation for the project 04-CC-17, PM 1.3 to 1.9, 47th Street to 6th Street in Richmond. Initial ground water quality studies were presented in "Report of Ground Water Investigation for the Proposed Richmond Semi-Depressed Section 04-CC-17", dated September 1978.

Initially, it was planned to conduct a three-phase ground water sampling and testing program over a three month period. This was extended to a six-phase study, involving a total of seven months. The ground water sampling was done by TransLab personnel. The testing for Phase I was done by TransLab Chemistry Laboratory in Sacramento. Phases II through VI testing was done by the Sanitation and Radiation Laboratory of the Department of Health in Berkeley, California. The tests were conducted according to methods prescribed in the Federal Register.

Ground water samples were taken six times at monthly intervals over a period of seven months. A total of 2,229 tests of various kinds were conducted, as shown in Attachment 1. Detailed tabulations of various test data are presented in Attachments 2 through 36.

A few samples were found to contain higher than normal (or allowed) quantities of pollutants or contaminants. As the wells from which these samples were obtained were subject to contamination from surface sources during the period of sampling, the high values are not considered to be representative of the ground water now contained within the shallow aquifers. The dewatering operation should eliminate these conditions.

METHODS OF DISPOSAL

During construction it may be necessary to remove from 2.5 x 10^6 to 3.5 x 10^6 gallons of ground water per day. The duration of the construction period is estimated at between 2 and 2-1/2 years. During this period the total pumpage in some reaches of the project could be substantially lower than at the start of construction. After construction the total pumpage would be reduced to the order of 1 to 1.5 million gallons per day.

The ultimate disposal of the ground water discharge was a concern to District personnel responsible for the project's environmental document. TransLab was asked to address the feasibility of various disposal strategies. Methods of ground water disposal considered were:

- 1. development of a freshwater marsh
- discharge into existing salt marsh(es)
- 3. highway landscape irrigation
- 4. direct discharge into San Francisco Bay
- use for human consumption

Due to the diverse disposal methods considered and their possible impacts on the environment, a series of meetings with appropriate State Agencies was initiated. Since the proposed disposal methods could affect public health, wildlife and habitat, and the San Francisco Bay environment, the California Department of Health Services (DHS), Department of Fish and Game (DFG), and the California Regional Water Quality Control Board (CRWQCB) San Francisco Bay Region were contacted. Meetings were subsequently held with representatives from each department to obtain their response to various proposed methods for ground water disposal.

REVIEW CONFERENCES

Department of Health Services, Berkeley (DHS)

On March 20, 1979, a meeting was held with Department of Health Services representatives. Representing the DHS was Mr. Dick McMillan, DHS Supervising Sanitary Engineer, and Mr. Bob Hultquist, DHS Associate Sanitary Engineer in the Richmond area.

After a review of the Phase I-VI water quality test data (appended) and a discussion of the impacts expected on the shallow aquifers in the project corridor, Mr. McMillan concluded the water is not suitable for human consumption. In addition to the water quality test data, which indicated some contamination, Mr. McMillan felt the soil depth over the shallow aquifer $(0-35\frac{1}{2})$ was not sufficient to ensure adequate filtration and natural purification processes. The shallowness of the aquifer precluded its use as a source for human consumption. (See References 2, 3 and 4.)

Mr. McMillan stated that there was no reason to preclude ground water from being used in highway landscape irrigation. After being informed that during part of the year roadway runoff will be mixed with the ground water for discharge from the project area, Mr. McMillan still felt that the water was suitable for highway right-of-way irrigation; but other uses, such as irrigation of parks, would require additional studies.

Mr. McMillan stated that the water might not be suitable for industrial utilization (e.g., Chevron of Richmond), because of relatively high total dissolved solids (TDS). This aspect of ground water utilization was not investigated

further because of the high TDS levels in the ground water as well as the additional contaminants expected from roadway runoff additions during the winter months.

It was noted that the Department of Health Service's responsibility did not extend to alternative disposal methods 1, 2, and 4.

California Regional Water Quality Control Board (CRWQCB), San Francisco Bay Region

On March 29, 1979, a meeting was held with representatives of the California Regional Water Quality Control Board, San Francisco Bay Region in Oakland. Attending for the CRWQCB were Messrs. Hobart C. Knapp and Richard K. McMurtry. These representatives were asked to evaluate the quantity and quality of ground water expected from the Hoffman project with respect to possible development of a freshwater marsh; discharge to an existing saltwater marsh; or direct discharge into San Francisco Bay via existing storm drains. (Alternatives 1, 2, and 4, Reference 5.)

Mr. Knapp outlined the Board's two main concerns in regard to the proposed Hoffman project:

- ° Possible effects of discharging freshwater into saline environments. Would discharge significantly affect the salinity of the receiving waters and result in adverse impacts to the aquatic environment?
- ° Protection of the aquifers underlying the project, particularly from saltwater intrusion.

EFFECTS OF FRESH GROUND WATER DISCHARGE

Various methods of fresh ground water discharge considered were as follows:

- ° Discharge into the Richmond Harbor Channel, or Inner Harbor Basin.
- ° Discharge across the Bay mud-flats via the existing Stege Drain near the U.C. Richmond Field Station.
- ° Development of a freshwater marsh using the ground water.
 - ° Discharge into the existing Hoffman Salt Water Marsh.

Mr. McMurtry noted ground water disposal into Richmond Harbor would be acceptable provided the discharge is at a sufficient depth to ensure adequate dilution and no significant salinity changes.

Mr. McMurtry requested a field review of the Hoffman Marsh area, with representatives of the Department of Fish and Game (DFG) to evaluate the remaining methods.

Mr. McMurtry noted the CRWQCB would utilize the Department of Fish and Game's expertise in marsh biology to determine the advisability of allowing any of the proposed methods of discharge.

After a field review of the Hoffman Marsh area, Fish and Game representatives Messrs. Mike Rugg, Bob Huddleston, and Ted Wooster stated that DFG would oppose ground water discharge into the existing Hoffman Salt Water Marsh.

There was no objection to the discharge of the ground water directly into San Francisco Bay.

There was no objection to the discharge of ground water into a freshwater marsh if one existed.

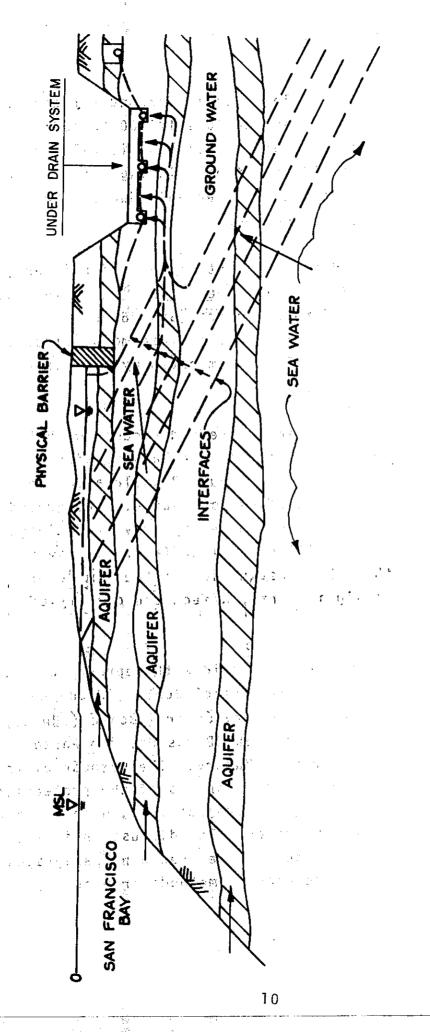
Both the CRWQCB and DFG stated that the discharge into Stege Drain would be acceptable and would result in no adverse effects on the creek or downstream tidal marshes and mud-flat environment.

PROTECTION OF THE AQUIFERS

A detailed literature survey was conducted to define the phrase "Richmond Aquifer" and was reported in Reference The important finding in Reference 1 was that the phrase "Richmond Aquifer" was vaguely used in the existing literature. The aquifers underlying the project were found to vary not only in thickness and extent but also in depth and characteristics. Hence, names were suggested for these various aquifers as noted in Reference 1 and as presented as Figure 1 in this report. The aquifers within the top 35 feet were termed "Hoffman Aquifers". These are the aquifers which will be subject to excavation on the subject project. The average excavation limit will be in the top $20' \pm$ for most of the project and at the deepest portion it will be in the top $30'\pm$. These shallow aquifers are subject to slow recharge and perched water table conditions.

The aquifers which extend generally from about 35' to about 125' were found to contain large amounts of water. These deeper aquifers are called "Richmond Aquifers" and will not be affected by the excavations for this project. These "Richmond Aquifers" should not be punctured due to any construction operations, including the subsurface drainage system.

The aquifers below 125'+ are called "San Pablo Aquifers". The lower extent of these aquifers has not been well defined. It is expected to be much greater than 300'. Very little information is available on the geohydrologic characteristics of these aquifers. During the seawater intrusion study, it was postulated, based on the Ghyben Herzberg Theory, that the depth to interface between seawater and ground water



SEA WATER INTRUSION STUDY, RICHMOND SEMI-DEPRESSED SECTION PHYSICAL BARRIER MODEL 4, LONG TERM EFFECTS OF A

FIGURE 2

From Ref. 1

Caltrans could induce some added seawater intrusion within the project area; which was, however, considered to be of no significant concern. The concensus was that there would be no damage to the aquifers in the Contra Costa Ground Water Basin as a result of the freeway construction. Mr. Richard McMurtry also suggested a monitoring system to evaluate the effects of the proposed construction. Mr. McMurtry noted no problems as far as SWRCB and CRWQCB are concerned and asserted he would confirm this decision by letter.

CONCLUSIONS

The discussions referred to above led to conclusions related to: (a) methods of disposal; (b) protection of the aquifers; and (c) a monitoring system. The conclusions are summarized for the first two subjects. The recommendations for the third section are presented in the end of this section.

Methods of Disposal

- 1. Discharge of the ground water to a freshwater marsh, (if one existed), would have been an acceptable disposal method as determined by the San Francisco Regional Water Quality Control Board. However, as the concept of developing a freshwater marsh as a mitigation measure is no longer under consideration, this method of disposal is discarded.
- 2. The San Francisco Bay Regional Water Quality Control Board acting on the advice of Department of Fish and Game representatives considers the discharge of ground water into the Hoffman Salt Water Marsh as unacceptable.
- 3. The California Department of Health Services representatives stated that the use of ground water for irrigation was acceptable only if the irrigation was limited to the highway right-of-way landscaping. Use of the ground water for other irrigation (e.g., irrigation of parks, etc.) would require further studies to assess its suitability.
- 4. The direct discharge of ground water into the San Francisco Bay was acceptable to the CRWQCB provided that any discharge into the Richmond Harbor would be at a depth sufficient to ensure adequate mixing and no significant salinity changes.

Discharge into the existing Stege Drainage Creek is considered acceptable by the CRWQCB.

5. Utilization of the ground water for human consumption was not acceptable to the California Department of Health Services.

Industrial use of the ground water was questionable.

Protection of the Aquifers

- I. Standards for discharging ground water into the San Francisco Bay Waters will be provided by the San Francisco Regional Water Quality Control Board. It is anticipated that there will be no difficulty in meeting those standards.
- 2. The proposed physical barrier on the bayward side and the underdrain system should arrest any onward progress of seawater and limit it to the confines of the semi-depressed freeway section.
- 3. Since all the dewatering facilities are to be placed at relatively shallow depths $(0-35\frac{1}{2})$, aquifers at depths below 35' in the Contra Costa Ground Water Basin (see Figure 1) will not be affected.

<u>RECOMMENDATIONS</u>

Monitoring System

- 1. Monitoring wells should be established on both sides of the depressed section to monitor any change in the quality of ground water.
- 2. The "Hoffman" and "Richmond Aquifers" should be monitored separately.
- 3. Spacing and depth of wells to the "Hoffman" and "Richmond Aquifers" will be decided by District 04 Materials personnel.
- 4. The quality of ground water in the "Richmond Aquifers" should be established prior to construction.
- 5. Any holes drilled into the "Richmond Aquifers" should be properly sealed or plugged to eliminate migration of ground water from one set of aquifers to another.

REFERENCES

- 1. John, S. B. P., Lee, A. Y., Leech, L. R., Campbell, J., and Macfarlane, J. G., "Report of Ground Water Investigation for the Proposed Richmond Semi-Depressed Section 04-CC-17", Office of Transportation Laboratory, Sacramento, September 1978. (not attached with this supplement)
- 2. Water Quality Appraisal Meeting with Department of Health-Hoffman, Memorandum, G. A. Winters (TransLab) to File, March 26, 1979.
- 3. Ground Water Investigation Richmond Semi-Depressed Section, Water Quality Study, Memorandum, S. B. P. John to R. A. Forsyth, April 9, 1979.
- 4. Ground Water Investigation Richmond Semi-Depressed Section Water Quality Study, Memorandum, R. H. Hultquist (Sanitary Engineering Section-SFBD) to S. B. P. John (TransLab), June 20, 1979.
- 5. RWQCB Meeting on Hoffman Groundwater Quality, Memorandum, G. A. Winters (TransLab) to File, April 10, 1979.
- 6. Water Quality and Discharge of Ground Water from Depressed Section-Hoffman, Memorandum, S. M. Shadle (Caltrans) to File, April 12, 1979.
- 7. Dewatering Discharge from Hoffman Corridor Depressed 'Freeway Section, Memorandum, Richard K. McMurtry, (CRWQCB) to Sid Shadle, Caltrans, May 3, 1979.

- 8. Meeting with RWQCB and Technical Staff, Memorandum, T. J. Walsh (Caltrans) to File, May 25, 1979.
- 9. Memorandum, from Richard K. McMurtry, California Regional Water Quality Control Board, San Francisco Bay Region, to S. B. P. John (TransLab) dated July 26, 1979.
- 10. Memorandum, from Richard K. McMurtry, California Regional Water Quality Control Board, San Francisco Bay Region, to S. B. P. John (TransLab) dated July 31, 1979.

State of California

Memorandum

: FILE To

Date:

March 26, 1979

File:

652907

From : DEPARTMENT OF TRANSPORTATION Office of Transportation Laboratory

WQ Appraisal Meeting with Department of Health - Hoffman

On March 22, 1979 Gary Winters accompanied Bennett John (Geotechnical Branch) to a meeting with Department of Health Services (CDH) regarding groundwater quality from the Hoffman Corridor semi-depressed freeway in Richmond.

Attending the Meeting:

Dick McMillian, CDH Supervisor Bob Hulquist, CDH District Engineer in the Richmond Area Tom Walsh, District 04 Hydraulic Engineer Richard Pence, District 04 Project Development, Project Eng. Bennett John, TransLab's Geotechnical Branch Bill Shoemaker, District 04 Environmental Planner Gary Winters, TransLab's Enviro-Chemical Branch

Tom Walsh outlined the Hoffman project and the following questions about the suitability of the ± 1 Mgd to be pumped from the aquifer.

- Suitability for use in a freshwater marsh
- 2. Suitability for use in a saltwater marsh
- 3.
- Suitability for irrigation Suitability for discharge into city storm drains and hence S.F. Bay 4.
- 5. Suitability for human consumption

After reviewing the Phase I-VI water quality test results (attached), Mr. McMillian concluded the water was not suitable for human consumption (coliform the main concern). McMillian indicated their responsibility did not extend to some of the other uses. John and I will write a confirming letter to McMillian, to which he will respond in regards to the unsuitability of this water for human consumption.

MEMO TO FILE March 26, 1979 Page 2

Mr. McMillian pointed out that their responsibility does not extend to some of the other uses noted above. As a result, additional meetings with DFB and the SFRWRCB will be scheduled to gain similiar acknowledgements concerning the suitability of the groundwater pumpings.

Tom Walsh and Dick Pence noted roadway runoff will be mixed with the groundwater discharge. After a short discussion of TransLab's findings from the 657117 project Mr. McMillian felt the water would probably still be suitable for highway irrigation, i.e., from a health point of view but probably not suitable for industrial use (eg. sale to Chevron in Richmond who buys 0.8 Mgd from the East Bay Municipal Utility District.

Currently, Bennett John and Gary Winters are scheduling meetings with SFRWQCB (meeting March 29, 1979 in Oaklnad) and DFG (to be scheduled) to appraise them of the Phase I-VI water quality test data. They will be asked to consider the suitability of the discharged runoff/groundwater for the remaining uses outlined earlier.

After the meeting with McMillian I approached Tom Walsh about modifying the Walnut Creek site for the 657305 project. He indicated he was familiar with the site and felt modification would not be much of a problem. Walsh requested a letter to Jerry O'Shea - District O4 Engineering Services explaining the project and requesting the necessary modifications to the Walnut Creek site.

Gary R. Winters Assoc. Environmental Planner

GRW:cj

cc: RHowell

RGilmore - HQ

state of California

Memorandum

Business and Transportation Agency

8-432-4721 S.B.P.John

Date: April 9, 1979

File: 04-CC-17, P.M. 1.3/3.9 47th Street to 6th Street 04209 - 108701

Lab. Auth. #652907

From : DEPARTMENT OF TRANSPORTATION

. Mr. Raymond A. Forsyth

Chief, Geotechnical Branch

Office of Transportation Laboratory

Subject: Groundwater Investigation of Richmond Semi-depressed Section Water Quality Study

On March 22, 1979, a meeting was held between regional public health engineers in the Department of Health, Berkeley, and representatives of District 04, as well as representatives from the Transportation Laboratory. The purpose of this meeting was to discuss the test data collected over a period of six months to determine the quality of the groundwater present within the shallow aquifers in the project area. These test data were generated to determine the potential uses of the groundwater in its present condition.

Those in attendance for the Department of Health included Dick MacMillan, Regional Engineer, and Bob Hultquist, District Engineer; Tom Walsh, Materials Engineer, Dick Pence, Project Engineer, Bill Shoemaker, Environmental Engineer, from District 04, CALTRANS; and Gary Winters and S. B. P. John from Headquarters Transportation Laboratory.

Mr. Walsh stated that the object of the meeting was to solicit the Department of Health for their opinion on how the groundwater from the Richmond semi-depressed section can be used. Mr. Walsh outlined the possible alternative uses of the groundwater:

- 1. Developing a freshwater marsh
- Developing a saltwater marsh
- 3. For irrigation purposes
- 4. Disposal into San Francisco Bay, and
- 5. For human consumption

It was agreed at the suggestion of Dick MacMillan that the idea of saltwater marsh should be explored further with the Department of Fish and Game and that the idea of disposing of the groundwater in its present condition into San Francisco Bay be dealt with with the Regional Water Quality Control Board in Oakland. In its present condition, the groundwater in the shallow aquifers is not deemed fit for human consumption.

Mr. Raymond A. Forsyth Page Two April 9, 1979

It was pointed out that after the semi-depressed freeway has been constructed, the surface runoff is likely to carry additional pollutants.

The waters "as is" can be used for irrigation on CALTRANS' landscape projects. The stormwaters during the winter may contain pollutants washed from the surface of the freeway which would not affect the usefulness for landscape irrigation purposes. Also, there may be no need for these waters for irrigation purposes during winter; therefore, alternate plans for disposal may have to be worked out.

S. B. P. John Project Engineer

SBPJ:bh

cc R. MacMillan

T. Walsh

W.Schoemaker

G.Winters

R.Pence

R. Prysock

Memorandum

To: Department of Transportation
Office of Transportation Laboratory
Att: S. B. P. John
Project Engineer
5900 Folsom Blvd.
Sacramento, CA 95819

Date: June 20, 1979

Subject: Groundwater Investigation of Richmond Semi-depressed Semi-Water Quality Study

From : Sanitary Engineering Section San Francisco Bay District

This is in response to your request for comments on your memorandum of April 9, 1979 regarding the meeting of March 22, 1979. Your memorandum accurately represents the view of the Department of Health Services on the disposition of the groundwater.

R. H. Hultquist

Associate Sanitary Engineer

RHH:gm

Memorandum

To MEMO TO FILE

Date: April 10, 1979

File:

From : DEPARTMENT OF TRANSPORTATION

Transportation Laboratory

Subject: RWQCB Meeting on Hoffman Groundwater Quality

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On March 29, 1979 Gary Winters accompanied Bennet John (Geotechnical Branch) to a meeting with the Regional Water Quality Control Board (Region 2) in Oakland concerning the groundwater quality from the Hoffman Corridor semi-depressed freeway in Richmond.

Attending the meeting were:

H. C. (Chuck) Knapp-San Francisco Bay Region Water Quality Control Board (Region 2)

The purpose of the meeting was to review the water quality data and establish the suitability of the groundwater for each of five disposal alternatives.

1. Discharge to a freshwater marsh

2. Flushing into existing salt marshes

3. Highway irrigation

4. Discharge into San Francisco Bay via existing storm drains

5. Human consumption

Tom Walsh briefly described the project and its groundwater problems and discussed the groundwater and water quality investigation undertaken by TransLab. Estimated water amounts vary from 2.5-3.5 mgpd during construction to 1 mgpd $(\pm 50\%)$ during the operational phase. Walsh also summarizes our previous meeting with the Department of Health Services (re: file memo 3/26/79, G. R. Winters) in which the Department of Health Services deferred responsibility on all the above uses except irrigation and human consumption to the RWQCB and/or Dept. of Fish and Game (DFG). Dept. of Health felt that the water was suitable for State highway irrigation and not suitable for human consumption (domestic and industrial)

Chuck Knapp outlined the boards two basic concerns:

- 1. Protection of the Richmond aquifer, particularly from salt water intrusion. The board have their geologist in Sacramento, Al Franks, to review the TransLab groundwater report and its aquifer protection proposals.
- 2. The possible effects of discharging fresh water into the saline marshes, especially during the summer. Knapp questioned that such a discharge might significantly affect the salinity of the receiving waters and result in adverse impacts to the aquatic environment. Knapp said the board would expect Caltrans to resolve this question with the Department of Fish and Game.

The question of Bay disposal of the groundwater was discussed with McMurty who does not foresee a problem with direct disposal to the Bay if the disposal is made in a sufficient depth of water to insure adequate dilution and no salinity changes (i.e. Richmond Harbor Channel or Inner Harbor Basin). The disposal of the water across the mud flats via drainage channels, i.e., Stege Drain, would require more detail and study to evaluate its impacts.

McMurty requested a full review with Mike Rugg of DFG to answer the question of discharge to the salt water marsh. Chuck Knapp indicated the board should be able to provide their comments shortly after Al Frank's review of the TransLab study and the DFG field review.

Gary R. Winters

Associate Env. Planner

REFERENCE 6

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Memorandum	FILE: 04209 - 108701 CC/Ala-I-180(17)
FILES	FROM: SID M. SHADLE
WHERE HELD BY TELEPHONE DISTRICT O	FFICE AT OTHER PARTY'S OFFICE STOTHER Field Site
INITIATED BY	DATE OF CONJENSATION
PARTICIPANTS NAMES	TITLES & AFFILIATIONS
Richard McMurtry Ted Wooster) Bob Huddleston) Mike Rugg) Joe Tieger Ken Wigglesworth Dick Pence) Roy Yokoi) Sid Shadle	Reg. Water Qual. Contr. Bd. (Reg. 2), Oakland (PWA) Calif. Dept. of Fish & Game (Reg. 3), Yountville (DFG) U.S. Fish & Wildlife Serv., Sacramento (USFWS) CALTRANS OEP, Sacramento CALTRANS 04, Proj. Dev. A, San Francisco CALTRANS 04, Env. Plng. Bch., San Francisco
	d discharge of groundwater from depressed section. 3/29/79, S. M. Shadle)

CALTRANS had requested comments from the RWQCB regarding five alternatives for disposing of groundwater from the proposed Hoffman depressed section. These choices, to be addressed in the water quality report being prepared by TransLab, are:

- 1. discharge to a freshwater marsh
- 2. flushing into existing salt marsh (cs)
- 3. use for highway landscaping irrigation
- direct discharge to S. F. Bay waters (via storm drain systems)
- 5. use for human consumption (domestic, industrial).

This review with DFG and USFWS was specifically requested by the RWOCB for the purpose of discussing the above alternatives and possible implications for natural ecosystems of the receiving waters.

We very briefly went through the 6-phase water quality data provided by TransLab. DFG commented that for the most part the water seemed "fresh." Wooster commented that the high coliform counts could indicate possible surface contamination of individual holes. Rugg noted that some data seemed particularly odd - possibly the result of uncased sample holes, poor sampling technique, or lab or recording errors. Specific parameters for which the data seems inconsistant include arsenic, lead, copper and sulphate (the latter can probably

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be explained by the strata in the test holes). Wooster asked where the 1 mgpd was coming from, how were the acquifers recharged and what effect would our pumping have on the aquifers. Dick Pence explained that the aquifers were quite small and perched and recharge was very slow; thus the +50% factor in the estimates.

I then recapped CALTRANS' mitigation and compensation proposals, stressing that we consider the efforts to rejuvenate Hoffman Marsh, improve tidal circulation and return portions of the S. P. levee to salt marsh to be appropriate compensation for the project's wetlands impacts. I added that we felt we had achieved basic agreement on those compensation concepts between USFWS, DFG, BCDC and ourselves.

I said that our current intention is to split the projected 1 mgpd (+50%) of groundwater to either end of the depressed section and discharge it to local storm drain systems (i.e.; Stege Drain near Bayview Avenue). If we encounter objections to discharge at this end (Bayview Avenue) we would probably pump all the water to the north end and discharge to the Richmond Harbor Channel. The five alternatives will be discussed in the supplemental water quality report but choices 1, 2 and 5 are not currently being contemplated.

Joe Tieger, said that USFWS agrees that compensation will be satisfied by our current proposals but he is still interested in creating a freshwater marsh. He wants to discuss the idea with various agencies and try to dig up the funds to purchase the necessary property. Dick Pence had asked R/W to develop some ball-park values for the land, which he provided to Tieger. Tieger said he would try to get some other government and public agencies together in a meeting sometime in the future to discuss his idea.

Dick McMurtry said that the RWQCB concerns centered around discharge across Bay mudflats or to tidal marshes. He agreed that our compensation seemed appropriate and said the Board would not expect a freshwater marsh unless necessary to effect treatment of the groundwater to satisfy DFG concerns.

Bob Huddleston said DFG favors improvement of tidal circulation in Hoffman Marsh but definitely would not want the groundwater discharged directly to the tidal marsh. Neither Rugg nor Wooster see any problem in discharging directly to the Bay or a freshwater marsh, if one existed. I noted that we could probably arrange to supply the pumped water to a freshwater marsh if one were created by others. Bob Huddleston asked what would be involved in pumping the entire 1 mgpd to the south end in such a case.

we walked along the SP levee and along Stege Drain downstream of the existing highway. All participants agreed that direct discharge into Stege Drain would not have any adverse effects on the creek or downstream tidal marshes and mudflats. Tieger asked if we could deposit the spoils from breaching the SP levee onto the resulting island to create some topograhic relief. This seems like a good idea and would solve the problem of a disposal site for the material.

Dick McMurtry said the Board would provide us with a letter addressing our five questions as soon as possible. They have only to receive the comments from their staff geologist on our proposals to prevent salt water intrusion before they respond.

I told all the participants that CALTRANS would contact them again when we reach the project design stage (possibly several years in the future) for assistance in developing the details of the marsh rejuvenation.

Selvishadle sid m. shadle

District Naturalist

SMS: em

cc: RIIJ-RWO-JWR-SMS, ROF-WRS, RDG-REF-RDP, TJW, K. Wigglesworth (OEP), G. Winters-B. John (TransLab), R. K. McMurtry (RWOCB, Reg. 2), T. Wooster (DFG, Reg. 3), M. Rugg (DFG, Reg. 3), B. Huddleston (DFG, Reg. 3), J. Tieger (USFWS)

OAKLAND 94607

CALIFORNIA REGIONAL WATER QUALITY CONTROL BOARD SAN FRANCISCO BAY REGION
1111 JACKSON STREET, ROOM 6040

Phone: Area Code 415 464-1255



May 3, 1979

File No. 2119.00 (RKM) vjw

Mr. Sid Shadle
Environmental Planning Branch
CALTRANS
P. O. Box 3366
San Francisco, CA 94119

Dear Mr. Shadle:

Subject: Dewatering Discharge from Hoffman Corridor Depressed Freeway Section

Based on our field inspection of the proposed discharge sites, review of the raw monitoring data, and conversations with Department of Fish and Game staff, I believe the location of your proposed dewatering discharge, either to the adjacent storm drain or to the proposed freshwater marsh, would not impair beneficial uses of the receiving waters.

Attached are the standard heavy metals limits for discharge to Bay waters. Please let us know if you anticipate any difficulty in meeting these limits.

The remaining issue to be resolved is the adequacy of your proposal to prevent salt water intrusion in the aquifers underlying the depressed section. We will be able to meet with you to discuss this aspect of the project in early May after reviewing comments prepared by the Technical Support Branch of the State Water Resources Control Board.

Sincerely.

RICHARD K. MCMURTURY

Rechard KM Menty

Water Resources Control Engineer

Attachment:

Heavy Metal Limits

cc: Mike Rugg, Department of Fish and Game, Yountville

Memorandum

: Files

Date: May 25, 1979

04-CC-17(180)-Rch File:

47th St. to Marine St.

04209 - 108701

Semi-Depressed Profile

Study

From : DEPARTMENT OF TRANSPORTATION

T. J. Walsh

Subject: MEETING OF MAY 17, 1979 WITH RWQCB AND TECHNICAL STAFF

Background

Several meetings with other State Agencies had been held with respect to disposal of ground water discharge from the proposed semi-depressed freeway profile through Richmond.

Certain issues previously had been resolved.

The purpose of this meeting was to discuss the following:

- Protection of the "Richmond Aquifer"
- Effects of discharging fresh water into salt water environments.

Meeting of May 17, 1979

The subject meeting was held in the Sacramento Office of the State Water Resources Control Board and lasted, uninterrupted, for approximately three hours (3930 - 1230).

Those in attendance were:

J. M	Í.	Parsons	r = ·	State	Water	Resources	Control	Board
------	----	---------	-------	-------	-------	-----------	---------	-------

R. McMurtry RWQCB (Oakland Office)

R. H. Prysock HQs Trans-Lab S. B. P. John HQs Trans-Lab

R. D. Pense District 04 - Proj.Dev. A D. G. Heyes District 04 - Materials T. J. Walsh District 04 - Hydraulics.

Mr. Walsh moderated the meeting and lead it off by reciting the history of the project over the past $25\pm$ years; noting the various concepts considered and studied, i.e.:

Files Page 2 May 25, 1979

- * A rolling grade line carried at ground level and rising over cross-street interchanges.
- * An elevated profile primarily on embankment.
- * A fully depressed profile 25 to 30 feet below ground level.
- * A fully elevated profile largely on structure.
- * The current semi-depressed profile nominal depth 10 to 15 feet below ground level; maximum localized depth 26 feet.

The several foundation investigations performed were covered in some detail, i.e.:

- * The exploration for embankment construction which was made in the latter 1950's and early 1960's.
- * The exploration for a fully depressed profile which was done in 1971-72. Discussion covered number and types of borings; number, extent and depth of pumping tests.
- * The exploration for a semi-depressed profile which was conducted in 1977-78. The number and types of borings together with the detail of pumping, recovery, and drawdown tests were presented and discussed.
- * The extent of data searching from both public and private sources was recited.

In the ensuing discussion, a number of specific items were covered, with agreements and conclusions as noted below:

- * Following the historical resume' and detail of exploration, Mr. Parsons evidenced satisfaction with the various pumping tests.
- Transmissibility values used were considered acceptable.
- * The concept of a physical ground water barrier on the bayward side was acceptable.

The possible occasion of "windows" in the aquicludes was discussed.

The linear extent of the barrier was agreed on at approximately Stations 200 to 260.

Files Page 3 May 25, 1979

Leakage around the parrier was of no concern.

- * It was concluded that "deeper aquifers" would not be affected. (Specifically those below a depth of 30 to 35 feet.)
- * It was concluded that, with appropriate control, discharge to the bay through either the Stage drain or into the Richmond Harbor would be acceptable.
- * Observation wells to both shallower and deeper aquifers will be incorporated. Spacing will be decided at a later date.
- * Water quality will be monitored after construction. Contingency plans will be developed should unacceptable contamination be detected.
- * Mr. McMurtry will prepare a set of water quality standards for discharge into the bay.

At the conclusion of the meeting both Mr. McMurtry and Mr. Parsons expressed satisfaction with the Caltrans report and with the Richmond project.

Mr. Parsons will prepare a re-evaluation for Mr. McMurtry.

After receipt of Mr. Parsons' comments, Mr. McMurtry will prepare a memorandum with the concurrence for Caltrans.

Tid Work

T. J. WALSH

District Hydraulics Engineer

TJW:ah

cc: RHPrysock
SBPJohn
RDPence
JO'Shea-DTCassinelli(2)
RAForsyth
TJWalsh

CALIFORNIA REGIONAL WATER QUALITY CONTROL BOARD

SAN FRANCISCO BAY REGION
1111 JACKSON STREET, ROOM 6040
OAKLAND 94607

Phone: Area Code 415 464-1255



July 26, 1979

File No. 2118.04 (RKM) aj

Mr. Bennett John
Department of Transportation
Transportation Laboratory
5900 Folsom Blvd.
Sacramento, CA 95819

Dear Mr. John:

Subject: Proposed Hoffman Freeway, Richmond, Contra Costa County

With respect to the subject project, I concur with the attached comments prepared by Mr. James Parsons of the State Water Resources Control Board staff. I see no problem with discharge of dewatering waters to either the Stege drain or a man-made fresh water marsh as proposed, provided the water quality limits listed in attachment B are met. Also, the proposed saltwater intrusion barrier appears adequate to prevent saltwater intrusion along most of the freeway depressed section. I do not consider continued intrusion in the small area between the Richmond Harbor and the west end of the freeway project to be significant, especially since there are no known beneficial uses of the area's shallow aquifers and the area already has evidence of intrusion.

Prior to final approval of plans and specifications, CALTRANS should submit to this office detailed plans of the dewatering and discharge facilities. Also, prior to construction, you should establish the ground watering monitoring wells specified in attachment A.

An NPDES Permit will be necessary for regulation of waste discharge during and following construction. This would set effluent limits on the dewatering discharge and regulate or prohibit the discharge of containinated stormwaters or other construction related wastes. Your application should be submitted 6 months prior to construction and should include a detailed description of erosion control measures during construction.

Sincerely,

RICHARD K. McMURTRY

Water Resources Control Engineer

Richard K.M.Murtry

Attachments (2)

A. Memo from Jim Parsons

B. List of NPDES Requirements

cc: List attached

cc: w/attachments

Sid Shadle CALTRANS P. O. Box 3366

San Francisco, CA 94119

Mike Rugg Department of Fish and Game P. O. Box 47 Yountville, CA

Attachment A

INTERNAL MEMO

In Reply Refer
To: 415/JMP

TO:D	<u>ick McMurtry</u>	<u> </u>		_ FROM:Ji	m Parsons	
S	an Francisco	Bay Regi	onal Board	DIVISION	OF PLANNING	AND RESEARCH
DATE:			· · · · · · · · · · · · · · · · · · ·	SIGNATURE	Jim	,
SUBJEC	T: Proposed	l Hoffman	and the second second		Contra Costa	

We met with representatives of the California Transportation Agency (see attached attendance list) at my office May 17, 1979, to discuss some of the potential water quality threats posed by the semi-depressed section near Richmond Harbor. In addition to my April 17, 1979, memorandum to you, I also prepared a list of discussion points (copy attached) prior to the meeting.

Findings:

- 1. Although there was only a fleeting reference to earlier pump tests in the September 1978 CalTrans report, the CalTrans' engineers also had available data from earlier full-fledged pump tests and 10 single-hole recovery tests to prepare estimates on the expected range of permeability values to be encountered at the project.
- 2. Since the September 1978 report, there have been a substantial number of additional groundwater samples taken and submitted for a broad spectrum of analyses. Results will soon be available.

Conclusions:

- 1. The methods used by the CalTrans' engineers to obtain permeability values for the shallow aquifers for estimation of dewatering quantities, settlement, etc., are reasonable.
- 2. The dewatering methods proposed by CalTrans probably will not cause serious water quality problems.
 - a. There will be induced seawater intrusion within a small area between Richmond Harbor and the west end of the freeway project. There are, however, no known beneficial uses of the shallow groundwater in this area.

1979

Carson 42479

/4CB 326 (3.75)

- b. It is quite possible that leaks in the cap over the deeper aquifers will be encountered during the freeway construction. If nothing is done, inflows from these "breakthroughs" will necessitate handling much larger quantities of water than expected and, in addition, lead to water quality problems. However, this situation will also seriously impede construction progress. Thus, CalTrans will have ample incentive to "plug leaks" as rapidly as possible. Methods available to them might include freezing of the soil, grouting to reduce the permeability, placement of a clay blanket, etc.
- Until the results of the recent analyses of groundwater are available, we cannot evaluate the impacts that the water removed by the dewatering facilities will have at the points of disposal. It does seem likely that the reported high coliform concentrations described in the August 1978 report were the result of contamination at the well rather than being representative of the water now contained in the shallow aquifers.
- 4. Since all dewatering facilities are to be placed at relatively shallow depths, there cannot be a serious "drying up" of the Richmond groundwater basin as a result of CalTrans' plans.

Recommendations:

Prepare waste discharge requirements for this project that contain:

- Limits on the specific constituents in the water to be discharged to the bay that could cause adverse effects.
- 2. Submittal of the detailed plans of the dewatering facilities prior to start of construction.
- 3. Establishment of monitoring wells on the landward side of the freeway semi-depressed section at a minimum of 2,000-foot centers between Freeway Stations 172+00 to 220+00; minimum of 1,000-foot centers between Stations 220+00 and 250+00; and minimum of 750-foot centers from Station 250+00 to 280+00.
- 4. Require CalTrans to contact the Regional Board at any time that inflows to the excavation and quantities of water removed by the dewatering facilities exceed that expected by more than 50 percent.

Attachments - 2

Attachment B

List of Probable NPDES Requirements:

			Average	Max	
1.	Suspended Solids	mg/l	30	60	•
2.	Oil and Grease	mg/l	10	20	:•
3.	Settleable Matter	m1/1	•1	•2 .	•
4.	рН				6.0 \pH<9. 0
5•	Toxicity	· .			90% survival (3 sample median)
6.	Coliform MPN/100ml				240 (5 sample median) 10,000 (verifiable max.)
7•	NH 40H mg/l				.025 mg/l annual median .4 mg/l max.
8.	Metals and Toxicants				Concentration not to be exceeded more than:

	Unit of <u>Measurement</u>	50% of time	10% of time
Arsenic	mg/l	0.01	0.02
Cadmium	mg/l	0.02	0.03
Total Chromium	mg/l	0.005	0.01
Copper	mg/l	0.2	0.3
Lead	; mg/l	0.1	0.2
Mercury	mg/l	0.4001	0.002
Nickel	mg/	0.1	0.2
Silver	mg/l	0.02	0.04
Zinc	mg/l	0.3	0.5
Cyanide	mg/l	0.1	0.2

Note: These limits would apply to the dry weather discharge. Modifications to certain parameters may be appropriate during wet weather. CALTRANS' application for NPDES permit should include an estimate of anticipated water quality during both dry and wet weather.

STATE OF CALIFORNIA-RESOURCES AGENCY

CALIFORNIA REGIONAL WATER QUALITY CONTROL BOARD

SAN FRANCISCO BAY REGION
1111 JACKSON STREET, ROOM 6040
OAKLAND 94607

Phone: Area Code 415 464-1255



July 31, 1979

File No.: 2118.04 (RKM)aj

Mr. Bennett John
Department of Transportation
Transportation Laboratory
5900 Folsom Blvd.
Sacramento, CA 95819

Dear Mr. John:

Though not stated in my letter of 23 July, my statement that an NPDES permit could be issued with the suggested limits is informal staff opinion only; issuance of a permit would be subject to both interagency review and our Board review which conceivably could result in modification of proposed limits or conditions of discharge.

Sincerely,

RICHARD K. McMURTRY

Richard K M Murty

Water Resources Control Engineer

ATTACHMENTS

RICHMOND SEMI-DEPRESSED SECTION WATER QUALITY TESTS - TOTALS

ATTACH. 1

Item	Phase I	Phase	Phase	Phase	Phase	Phase	others*	1 20000
		П		IA	X	VI	orners	Total
Atrazine				. 1				1
Endrin	9		17	12				38
Lindane	9		17	12				38
Methoxychlor	9		17	12	_			38
Toxaphene	9	-	17	12	_	_		38
2,4-0	9		17	12				38
2,4,5-TP SIIVEX	9	-	17	12			. <u> </u>	38
PН	9	10	17	16	17	17	17	103
TDS	9	10	15	16	17	17		84
Conductivity	9	10	16	16	17	17		85
Chloride	9	10	17	16	17	17	17	103
Sulfate	9	10	17	16	17	17	17	103
Arsenic	harres	10	17	16	17	17		77
Barium		10	16	16	17	17		76
Cadmium		10	17	16	17	17		77
Chromium		10	17	16	17	17		77
Lead		10	16	16	17	17		76
Mercury	9	10	15	16	17	17		84
Nitrate	9	10	17	16	17	17	4	90
Selenium		10	17	16	17	17	_	77
Silver		10	17	16	17	17		77
Coliform	9	10	17	16	17	17		86
Fecal Coliform		10	3	,	17	17		48

RICHMOND SEMI-DEPRESSED SECTION

ATTACH. 1

WATER QUALITY TESTS - TOTALS

Item	Phase I	Phase II	Phase III	Phase IV	Phase V	Phase VI	others*	Sub- Total
Magnesium	9	-		16	16	17		58
Calcium	9			16	16	17		58 73
Bicarbonate	9	10		16	17	17	4	73
Potassium				16	1.7	17		50
Fluoride	-	10		16	17	17		60
Iron	9	286, ed.	16	16	17	17		75
Sodium	9			16	17	47		59
Zinc	9		17	16	17	17		76
Manganese	9		16	16	17	17		75
Copper	9		17	16	17	17		76_
Resistivity							17	17
Totals	198	180	419	474	440	442	76	2229

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* Pre-Phase I tests

ATTACHMENT 2

ARSENIC - MG/L

	BORING	PHASE I	PHASE II	PHASE III	PHASE IX	PHASE Y	PHASE XI	REMARKS
L	R-1	\	`	910.	.033	0.005	800.0	
	R-2		`	<.00.	.002	100.>	200.0	
	R-2A		\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	<,0025	100.>	0,0025	200.0	•
	P-12			0.52 ?	400.	100'>	900.0	
	P-1		.002	toa.		0.040	0.003	-
	D-17		400°.	t-00°.	.000.	0.016	6,009	
	91-Q		002	.003	. 003	0.100	0.007	
	D-10	-	.002	.002	.002	0.003	900,	
	P-9		.002	2005	.005	200.0	500	
	R-3			.007	7,00.7	0.002	200	
	P-7		100.	200.	00	/00.>		
	P-6		100	. 003.	9	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	0.000	
	+-d		100.	- <u>ō</u>	.00	7.001	100, 7	
	P-2		100	600	8	⊅00.0	400.0	
	R-4			8,	ō	0.007	, 6 7	
	P-13		100	200	100.	0.00	0,00	
	8-5			1500	<,001	100.7	0.002	
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ATTACHMENT

BARIUM - MG/L

Boring	PHASE I	PHASE II	PHASE III	PHASE IV	PHASE X	PHASE XI	REMARKS	
R-1			107	40.1	1.0>	0,066		1
R-2			80	× 0. –	<0·I	680.0		•
R-2A			240.	~o>		0.069		
P-12		•	0	<u>o</u>	0	0,12		
- - -		0.36	*		0.60	0,12	* Insufficient	
D-17		. 0.76	0.7	ō	0.30	<i>\$1.0</i>	sample	
91-Q	•	0.23	- 0	, o .	0.6.0	0.097		
P-10		0.24	= 0	•	1,0>	07.0		
P-9		0.57	o W	ō	. <u>Q</u>	0,0,55		3 2,
R-3			08.0	- 0 V		0.057		
P-7		0, 72	6.75	-0) o V	0,067		
9-d		0.17	เจ๋	Ġ.	<i>o</i> .	#/		
p-4		50 54	Š	< O. I.	~ V	60.0		
P-2		0.29	o.	-0	o. Ø	0		
R-4			0.24	- 0 V	0 Z	0.033		
P-13		0.28	0.20	.0>	, , ,	0.067		
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								<u>.</u>
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ATTACHMENT 4

CADMIUM - MG/L

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REMARKS	SYNERGIATIO	W/ZINC -	.03 CD + .15 Z	TOXIC TO SALMON	. Y .													* ** ** ** ** ** ** ** ** ** ** ** ** *				
PHASE XI	0.007	0.00)	7.007	100.>	0.003	0,002	6000	. 700.	100	000	6,00	1001>	- 00 00 V	00	000	700	· ·	3,			
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Boring	R-1	R-2	R-2A	2	4	=	D-17	91-Q	P-10	P-9	R-3	P-7	9 - d	p-4	P-2	R-4	P-13	10				

CHROMIUM

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ATTACHMENT

MG/L

BORING	PHASE I	PHASE II	PHASE III	PHASE IX	PHASE X	PHASE VI	REMARKS	
R-1			hoo.	<.005\ S005\	900.0	0,033		-
R-2			<oo.></oo.>	2.005	0.007	0.005		
R-2 A			100.	.005	0.015	0,005		
P-12	p land		.072	.005	0.008	0.008		
		<.02	+o.>		0.600	800'0		
D-17	air a	<.02	≯0. >	700.	0.058	5/0'0		
9i-q	The Section 1	< .02	0.023	0.01	0.260	110.0	-	
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P-9	And the second of the second o	<.02	.027	0	0.020	5,005		
R-3		The first of the control of the cont		<.oo.		0,00%		
P-7	13	×.02	0	500.	0.005	0.003		
P-6		20,	710	×.00.×	. K. 005	0,007		
P - 4		70	0.60	6.52	0.012	0.0		
P-2	* · · · · · · · · · · · · · · · · · · ·	7 02	120	\$ \$ \$	900.0	0.07.7		
₹-¥			×0.	900	460.0	0,017		
P-13		< .02	7.0	7.00.5	0.0.0	0.002		** - ** *** - * *** - * *
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ATTACHMENT 6

LEAD - MG/L

BORING	PHASE I	PHASE II	PHASE III	PHASE IV	PHASE Y	PHASE XI	REMARKS
R-1			010.	0.024	0.010	0,072	
R-2			2005	0.010	7000	000	-
R-2A			600	7000			
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F- 12			. 280	0.13	0.016	1,000	
<u>-</u>		.026	.]	•	1.400	0,020	
D-17		890.	900.	0.018	0.050	0.057	
91-Q		.025	.025	0.022	0.012	6200	
P-10		.005	.036	0.07	0.080	0 0	
p-9		+ 00	030	0,07	0 0 0 0) /	
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9-d		.003	050	20	0.005	0.021	
p-4		900.	024.	6,013	<.005	9000	
P-2		300	80	0.005	0.005	0.04	
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P-13	ora e e e e e e e e e e e e e e e e e e e	800	0 7 0	0.005	0.007	2005	
in &		-	890	/00.>	0.005	0.020	
				•		}	
	-						
							MAX. CONTAMINANT
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ATTACHMENT 7

Boring	PHASE I	PHASE II	PHASE III	PHASE IV	PHASE Y	PHASE XI	REMARKS	· · · · ·
R-1			100	9000.	8000.	4,000,0		1
R-2			.0005	9100.	1000.>	4000.		
R-2A			.0003	9000.	<.0001	2000		
P-12			*	.0002	5000.	.0003	* Insufficient sample	-3
	<.0002	.0002		13 13 13 13 14 15 16 16 16 16 16 16 16 16 16 16 16 16 16	0/00:	1000		· 交易
D-17		+000.	<.0001	.0003	.0003	7,000,7		
91-Q	<.0002	.0002	(000'>	.0003	£000°	1000		
D-10	<.0002	.0002	:0003	(000°)	,0002	2000.		
P-9	<.0002	1,000.>	/000/>	1000	.0003	1000.>		
R-3			×.000	.0003	1000.>	.0002		
P-7	<.0002	.0003	1000	2000	<boo!< th=""><th>2000</th><th></th><th>- 1</th></boo!<>	2000		- 1
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P-2	<.0002	,000i	1000	2000	t000.	1000		
R-4			(000,	9700.	1000	8000		2
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2-5			.0002	.0003	/000'>	4000		4. W
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ATTACHMENT 8

NITROGEN - MG/L

BORING	PHASE I	PHASE II	PHASE III	PHASE IV	PHASE X	PHASE XI	REMARKS
-R	Nitrate	Nitrate	1.0>	0.3	0.3	1.57	SEE NITRATE
R-2	Ser trees		7	7,7	Ŋ	ţ	FOR STANDARD
R-2A		-	ω, ω	2.9	3.0	•	
P-12			<,002	~ =	10.6	6.0	
P-11	0	5.3	54 00		<i>w</i>	w O	
D-17	.· .•	φ, 15	100.	9	1.2	0,7	
D-16	28	7	ls:	5.0	5.6	7	
P-10	24	7	4	<i>1</i> 0	6.4	<i>w</i>	
P-9	32	26	, 6 (3)	9.9	9	4	
R-3			ó	5	0.2	- 00	
7-q	20		ò	9	2.0	Ò	
9-d	27	N N	SQ In	- Vi	vi.	91	
4-4	7	22	500	6	5.7		
P-2	Ŧ		, , , , , , , , , , , , , , , , , , ,	- 60	∞ 0.	00	
R-4			<0.I	, 0	 	4	
P-13	7.	48	0.80	<u>.</u>	8.6	- 00	
Z-5		· ·	1.0>	0,	0.7	7	
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Boring	PHASE I	PHASE I	PHASE III	PHASE IV	PHASE X	PHASE XI	REMARKS	
R-1			44·0>	5,8	iQ 80	7,5		
R-2		-	#	9.	2)	28		
R-2A			<u>vo</u>	ū		7.7		·
P-12	٠.,	-	<.009 ?	29	47	39	₹ 507	
=	0	5.3	7		±	<i>a</i>		<u></u>
D-17		5	t100°	2.7	N W	20		
D-16	28	24	9	9	25	Ō		
P-10	7	7	0 -	20	22	9/		·
P-9	32	26	. 69 . 60	9.	27	/3/		`
R-3			ナ世・0	7#:0	989	69		* 1.1.1
p-7			##.>	4	00	<u> </u>		5 - Jah.
9-d	7	- 23	. N	6	62	7		
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ATTACHMENT 10

SELENIUM - MG/L

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	Boring	PHASE I	PASE II	PHASE III	PHASE IX	PHASE Y	PHASE VI	REMARKS	
	R-1			.01.2	100.7	900.0	<,002	4)
	R-2			\ \ \ \ \ \	100.7	100.>	500'>		••
	R-2A		-	100.V	100.>	. 100.>	200.0		
	P-12		•	<.002	- - - - - -	100">	Z00. >		
	=-4		100.	100:>		0,0,0	<,002.		٠.
	D-17		.003	100'	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	\	×.002		
	91-Q		100°	/00:>	100.>	100°.>	×.002		
	P-10		.003	īgo. >	100.	100.>	0.004		
:	P-9		003	, 6 0.	100.	100.	200">		
	R-3			, 0 0	- 00. V	100.	, 0, 2,		
	P-7		.002	400.	4,001	100.	200.		
	P-6		2002	io V	/po:>	100.2	×,002		
	p-4	-	Job		0 V		K.002		
· .	P-2		,do3	- - - - - - -	ō V	-00°.	7.00.7		
,	₩-X			005	- <u>o</u>	8	6000		<u></u>
• :	P-13		003	100:>	, 00.	8.	, v , v , v		<u> </u>
	75-55 15-	•		100.>	100.>	100°>	<.002		
		•			-				
· · ·									
									
=						The same and same and same and	Anna de la companya d		Ť

ATTACHMENT 11

SILVER - MG/L

R-2 C.005 C.001	BORING	PHASE I	PHASE II	PHASE III	PHASE IV	PHASE Y	PHASE XI	REMARKS	
\$\\ \chinar\china	R-1			<,005	<0.010	100.>	100'>		1
\$\infty\$ \chinar\	R-2			د. ر <u>ه</u>	100.0>	<.00!	100.>		
Cool	R-2 A			<.10	100.0>	100.>	100'>		
Cool	7-12			.002	<0.001	<.00 l	100'>		#1.
1000 1000	1 -d		< 0.01	Ÿ	DRY	0.002	100.>		
Co.0	D-17		<0.01	\$00°.	<0.001	<00 <i>I</i>	100.>		
COO CO DO	91-16		< 0.01	ÿ	< 0.001	0.00/	100'>		
	P-10		<0.01	< 0.10 10	0.028	0.00.	1000		
	P-9	• •	10:0>	0 . 0 V	<0.001	100°	100,7		
1000 1000	R-70			0,0	<0.00	8	100">		
\$ 000 \ \$ 000	P-7		10.0>	01:0 V	* 00.00	, 0 7	100">		
1000	9-d		1000	<0.10	K.00.1	, 00.X	/00·>		- 10
(0.00) (0.00)	7-4		10.0>	× 0.10	<0.001	9,00	700,2		**************************************
\$\frac{20.00}{20.00} \	p-2		<0.01 VO.01	<.o.10	<0.00 E	- 00. V	1,00,		
100.0 <0.001 <0.001 <0.001 <0.001 <0.001 <0.001	R-4			ر م. 6	<0.001	00.0	(0°)		• · · · · · · · · · · · · · · · · · · ·
700.7	P-13		\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	<0.10	<0.001	0.00[0.001		# 1
	15 - S			<0.10	700.>	<.00.>	7,00,5		
		·							•
				·	•				. ,
				-	- 7	- 1	- 4		

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ATTACHMENT 12

TOTAL DISSOLVED SOLIDS - MG/L

	BORING	PHASE I	PHASE II	PHASE III	PHASE IX	PHASE I	PHASE XI	REMARKS
	R-1			22188	27869	27620	3520?	
:	R-2			543	4/5	536	787	
	R-2 A			<i>w</i>	356	307	322	
	P-12	,		769	. 527	530	125	-
	H4	396	443	*	DRY	†	425	* Insuff sample
	D-17		359	160	298	82.89	575	
	91-0	544	475	292	421	428	340	
	P-10	417	451	715	10 10	345	7/5	
	P-9	548	816	774	739	725	00ħ	
	R-3			<u>w</u>	<u>w</u>	282	<i>w</i> 00	
	P-7	3/2	345	30	38	310	w 70	
	P-6	524	336	457	469	460	15.32	
	p-4	383	463	30	305	00.	- 0 - 0 - 0	
	P-2	643	9	. o . o	#29	588	24.00	
· .	4-4	- >			29405	29/55	2/720	
	P-13	80₩	906	7 2 20	40 60	855	9	
	7. 10	-		550	509	529		
·								
Ţ								1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -

Contract.

CONDUCTIVITY - MMO/CM

Boring	PHASE I	PHASE II	PHASE III	PHASE IX	PHASE X	PHASE XI	REMARKS	
R-1			1157/38220		41100	5820 ?		}
R-2			0001/466	242	(080	th-L		
R-2A			405 1286	570	069	530		
P-12			809 7 975	146	186	7.60		
- - -	089/899	* 420/700	**	elike E	011	£25	* Jartek V shield	
D-17	7	4557580	544/ 593	.598	643	576	Total removed	14 (14) (14) (14) (14) (14) (14) (14) (1
91-Q	726/740		800/ 762	771	840	787	1007	
P-10		*##/720	763/ 718	721	700	752		
P-9	005/1370	*+38/1310	1337/1362	1390.	1210	465		
R-3			688/630	9	582	0		
P-7	553 / 530	338/535	612/570	575	206	27		
P-6		*362/830	891/817	87.2	86.2	60		
P-4		411/640	722/666	629	6	760		* * * * * * * * * * * * * * * * * * *
P-2	1086/1060	41501020	1106/1080	1065	139	7		
R-4			1,428,0	74400	08/97	32500		* * *
P-13	1449/1330	* 408/1410	1112/1740	1500	800	0891		* * .
10.			1940/ 1041	939	1020	7.97		
				-			•	-
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		-	-					d

The state of the s

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	ATTACHMENT	NT 14	5	CHLORIDE	T FVETC				
						M.47. L			1
	BORING	PHASE I	PHASE II	PHASE III	PHASE IZ	PHASE V	PHASE XI	REMARKS	
	1-4			11903	17521	15803	18307	H000 M67-1	1
1	R-2			93.1	7.99	876	7.79	FOR GASS, PIKE	
	R-2A	. 1 		75.3	73.6	67.8	50.5	# PERCH HOOME	
	P-12			90.7	916	92.4	77.0		
	=	09	72	45.2	ጋሌ ጉ	101.9	70.9		: .
	0-17		25	55.2	63.9	60.0	53.00		
	D-16	65	74	83.5	- 276	92.4	72.7	- 1	
J- 3	<i>P-</i> 10	67	779	577	78.3	75.0	56.2		:
	b-d	911	511	124	19.6	123.5	25,3		
	ج- ش-			56,1	56.8	47.1	23,4		
	2-4	1.00	9.2	1.91	23.0	74.4	127		
1	P-6	87	QQ	61.5	1.56	7 70	1 (
-	3-	73	89	83.2	823	٤ 78	707		
	2	1	1139	153.7	0.2.7.1	153.2	- 1 5 0 0		
	R-4			14537	5668	17010	11470		
	P-13	172	197	2[]	249.9	219.5	751		
	R-5			129.6	9.601	136.4	£2.3		
			* * *						:
				, , ,	+				•

R-1 Fuse I Phase II Ph	A B C	Þ		REMARKS
65 55 56 140 93 87 71.2 93 87 71.2 139 137 720.6 123 440 35.2 123 147 127 123 147 127	6 W	0.200		
52.5 65 56 39.2 65 56 39.2 71.2 38 38.2 71.2 39 40 53.1 70 70 53.1 71.2 34.8	vo :	0000	221.7	40.5 MG/L
56 55 56 39.2 38 38.2 38 27.3 38 27.3 42 44 43.2 70 70 53.1 70 70 53.1 70 36.2 71 34.8	7	120	94.2	WILL NOT SUP-
65 56 56 39.2 93 887 71.2 38 27.3 42 44 37.4 67 70 53.1 70 70 53.1 71 127 127 1276	*	25.9	21.9	G-ROWTH.
65 56 39.2 93 87 71.2 38 27.3 139 137 120.6 70 70 36.2 176 53.1	٠	120	121.8	-
38 38 27.3 38 38 27.3 139 137 120.6 70 70 36.2 175 175 1776 1776 1776 1776 1776 1776 17	. 7	125	80.0	
38 38 38 139 123 470 470 470 470 123 123 123 123 123 123 123 123	9	18,4	16.4	
38 38 27.3 42 44 43.2 70 40 36.2 70 70 53.1 123 34.8	· ·	66.0	68,5	
139 42 44 524 70 70 70 70 70 71 71 71 72 73 74 75 76 77 77 77 78 78 78 78 78 78 78	70	38.0	24.7	
42 42 44 37.4 40 40 40 40 40 36.2 40 40 53.1 40 53.1 40 34.8	9	155	58.6	
42 67 70 70 70 70 70 70 70 70 70 34.8		48.0	31:0	
34.8 34.8 34.8 34.8		58,0	0.1.0	
39 40 36.2 70 70 53.1 123 147 127 34.8		80	7,	
70 70 531 1776 123 147 127 34.8		Ž Ž	60 00	
123		77.0	S S S	
123 147 727		2 400	042/	
34.8	2	160	200	
	· •	001	35.0	
	-			
	-		··	

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ATTACHMENT 16

ENDRIN - MG/L

	7 - ()	PHASE I	PHASE I	PHASE II	PHASE IV	PHASE V	PHASE TI	REMARKS
-	1-8				* 1007 /			
	-			* -000.	¥ 1000'Y			נו נו
:	R-2			1000:>				CELECTION CIMITS
	R-2A		-	\ .000 \	ار در	•		
	P-12			1000, >	3			
	<u>-</u>	10000		1000. >				
	D-17			1000:>		:		
	91-0	10000		1000:>				
	P-10	.00008		1000.>				
:	P-9	-0000		/,000; >				
ت بر.	R-3			7000.>				
	P-7	0000		000;	A company of the comp			
٠.	D -0	10000		7000:>				
	P-4	0000		000:				
-	P-2	- - - - - - - - - - - - - - - - - - -		000				
	R-4	The second secon		000	and the same of th	and the same		
•	P-13	10000·		- 000 0. V				
<u> </u>	10 02			1000.				
٠					*		•	MAX. CONTAMINANT
								LEVEL = 0.002

BORING	PHASE I	PHASE II	PHASE III	PHASE IX	PHASE X	PHASE XI	REMARKS
A 2 - 1 - 0 - 1 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2	* * * * * * * * * * * * * * * * * * * *		*	* 000			MAX. CONTAMINANT LEVELL = 0.004 * LEVELS AT OR BELOW DETECTION LIMITS
			 				-

BORING	PHASE I	PHASE II	PHASE III	PHASE IX	PHASE Y	PHASE XI	REMARKS
R-1			* 00. >	* 100.>			MAX. CONTAMINANT
R-2			*				LEVEL = 0.1
R-2 A			4.4				
P-12			*	77			
-	*	44.74	<u></u>				* LEVELS, S
D-17					-:	-	DETECTION LIMIT
91-0	*						
P-10	*		**	· ·		- - - - - - - - - - - - - - - - - - -	
P-9	*		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	• • • • • • • • • • • • • • • • • • •			
R-3							
P-7							
P-6	*						
p - d	*					1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	
p-2	*			_			
R-4							
P-13	*						
7. 10							
	-						

	ATTACHMENT	61 11		TOXAPHEINE	MG Z				
	BORING	PHASE I	PHASE II	PHASE III	PHASE IV	PHASE V	PHASE I	REMARKS	
	R-1			* 100.7	* 100.7			MAXIMUM CONTAM-	
	R-2A P-12 P-11	*		* * *	* *			O. OOS	
56	D-17 D-16 P-10	*		* *					
	P-9 R-3 P-7			* * * *	*				
	7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7			* * * *					

ATTACHMENT 20

2,4-D - MG/L

!	+	······································														·		· · ·			1
REMARKS					* LEVELS. <	DETECTION LIMITS				•									MAX. CONTAMINANT	LEVEL = 0.1	07.6 7 7.00
PHASE TI						ē.										: ·					
PHASE I																					
PHASE IV	* 1000.>		*	=		\$		=			3	*	. 2	•	7	1	=		:		Martine :
Рнаѕе III	× 1000.>	-	→	=	-	=		~			Z	Ī	: :	*	. 3		1	, bir (A) inflamen gaze agant dipart			The start
PHASE II			-				A STATE OF THE STA		:			! :									
PHASE I					*	:	*	*	*		*	*	*	*		*					9x3/24/17
BORING	ج 	R-2	R-2A	P-12	=	D-17	D-16	D-10	P-9	٦- س-۵	P-7	D-6	7-4	p-2	R-4	P-13	م- ال		. > 2		

ATTACHMENT 21 2,4,5

2,4,5-TP SILVEX -- MG/L

T	<u> </u>		ું			14 30					·	·	-				
REMARKS				* LEVELS S	DETECTION LIMITS								:				MAX. CONTAMINANT
PHASE VI					1		*					•					
PHASE V					i i	37	1			er inse							
PHASE IX	* 1000.>	***	1	9.3	±	*				.=	=	3	**	•		*	
PHASE III	* - 000.	**************************************	* **	*		. 3	22	-	: : ::::::::::::::::::::::::::::::::::		,	e'				÷	
PHASE II				-									\$ 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	* .	2	- -	
PHASE I				*		*	*	*		*	*	*	*		*		
BORING	R-1 R-2	R-2A	2 - d	<u>-</u>	D-17	D-16	0 -d	010	R-3	7-d	9-0	4-4	P-2	R-4	P-13	in L	1

ATTACHMENT 22

ATRAZINE - MG/L

RKS			
REMARKS			
Рназе 🗵			
PHASE V			
PHASE IX			ر. مم. ک
PHASE III		·	
PHASE II	1		
PHASE I			
Boring	R-2 R-2A P-12	- 10 0 1 d d d d d d d d d d d d d d d d	

0.09 0.08 0.08 0.08 0.06 0.06 0.06 0.09 0.09 0.09 0.09 0.09	R-1 .09 0.08 0.25 R-2A <.06 <.05 <.05 R-2A <.06 <.05 <.05 P-12 <.06 <.05 <.05 P-13 <.00 <.05 <.05 P-14 <.06 <.05 <.05 P-15 <.05 P-16 P-17 P-19 P-19	# 0.0 0.0 0.0 0.0		PHASE IV	PHASE Y	PHASE XI	REMARKS
R-2A <.06 <.05 R-2A <.06 <.05 P-12 <.05 <.05 P-11 <.004 <.05 <.05 D-16 <.004 <.06 <.05 P-10 <.005 <.05 <.05 P-10 <.05 P-10 P-10 P-10 P-10 P-10 P-11 P-12 P-13 P-13 P-13 P-13 P-13 P-13 P-13	R-2	70.0 70.0 70.0 70.0	5	90.0	0.25	<.05	
0.04 0.05 0.06 0.06 0.07 0.07 0.08 0.08 0.09 0.09 0.09 0.09 0.09 0.09	0.04 0.05 0.05 0.09 0.06 0.05 0.02 0.06 0.05 0.02 0.06 0.05 0.05 0.06 0.05 0.06 0.06 0.05 0.07 0.06 0.05 0.06 0.06 0.05 0.07 0.06 0.06 0.06 0.06 0.06 0.07 0.06 0.07 0.07 0.07 0.07 0.08 0.09 0.07 0.09 0.06 0.07 0.06 0.07 0.07 0.07 0.08 0.09 0.09 0.09 0.09 0.09 0.09 0.09 0.09 0.09 0.09 0.09 0.09 0.09 0.09 0.09 0.09 0.09 0.09 0.09 0.09 0.09 0.09 0.09 0.09 0.09 0.09 0.09 0.09 0.09 0.09	0°0°0°0°0°0°0°0°0°0°0°0°0°0°0°0°0°0°0°	×.06	<0.05	۲,05	<.05	
0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.04 0.05 0.06 0.06 0.06 0.06 0.07 0.06 0.06 0.06 0.07 0.08 0.08 0.09	0.00 20.00 20.00 20.00 20.00 20.00	90.>	<0.05	<.05	<.05	
P-II 0.04 D-I7 0.06 P-I0 0.00 R-3	P-II 0.04 D-I5	40.0 0.0 20.0 20.0 20.0	\$0.>	<0.05	<,05	2.05	
D-17 D-16 0.0 C.06 0.05 P-10 0.02 P-4 0.02 R-3 0.02 R-3 0.05 P-4 0.05 R-3 0.05 R-4 0.05 P-4 0.05 P-4 0.05 P-4 0.05 P-4 0.05 P-4 0.05 P-4 0.05 P-7 0.05 P-4 0.05 P-4 0.05 P-4 0.05 P-13 0.06 C005 C005 C005 C005 C005 C005 C005 C005 C006 C005 C006 C005 C007 C005 C006 C005 C007 C005 C008 C005 C009 C005 C006 C005 C007 C006 C007 C007 <t< td=""><td>P-17 P-16 0.0 C.06 C</td><td></td><td>90.7</td><td>-</td><td>00</td><td>20.></td><td></td></t<>	P-17 P-16 0.0 C.06 C		90.7	-	00	20.>	
0.00 0.005 0.0	0.00 0.00	:	% V	<0.05	<.05	20,2	
0.02 0.04 0.05 0.05 0.06	0.02 0.06		<.06	20.05	- 0	<,05	
0.02 0.04 0.05	0.02 0.06		90.0	<0.05	<.05	50.0	
7.0.0.0 7.0.0.0.0 7.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0	0.0.0 0.0.0 0.		> 0.06	<0.05	. ä	<.05	
0.00 0.00	0.02 0.02 0.02 0.04 0.05		×4.06	N 0 0		o.os	
0.02 0.02 0.02 0.05 0.05 0.05 0.05 0.05	0.02 0.05		Ó-	X. O. O. O.	<0.0 <i>5</i>	20.5	
0.00 0.05 0.05 0.05 0.05 0.05 0.05 0.05 0.05 0.05 0.05 0.05 0.05 0.05	0.02 0.06 0.05 0.06 0.07 0.09 0.09 0.05 0.04 0.05			6 0 0	. la 0 V	90,0	
0.02 0.05 0.05 0.05 0.05 0.05 0.05 0.05	0.02 0.05		∴. o ́	\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	× 45	₹.05 .05	
\$0.0 \$0.0 \$0.0 \$0.0 \$0.0 \$0.0	\$0.0 \$0.0 \$0.0 \$0.0 \$0.0 \$0.0 \$0.0 \$0.0		90.0	<0.05	50.5	0.20	
\$ 0.0 \$ 0.0 \$ 0.0	\$0.0 \$0.05 \$0.05 \$0.05 \$0.05		60	0.05	0.14	, ds	
	< < 0.05 < < 0.05 < < 0.05	Ö	\$0.0¢	<0.05	<.05 <.05	اه ک	
< 0.06 < 0.05 < 0.05		is a	90,0 ×	<0.05		\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	

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ATTACHMENT 24

IRON LEVELS - MG/L

		-						
	Boring	PHASE I	Phase II	PHASE III	PHASE IX	PHASE X	PHASE VI	REMARKS
	R-1			1.28	0,53	1.03	2.55	1-2 MG/L LETHAL
	R-2	· · · · · · · · · · · · · · · · · · ·		~: 00	90.0	90.0	0.52	A PERCIT AT BH
	R-2A	:		.02	3.99	1.26	1.59	5.0 TO 6.7
	P-12			1	.00 .00	6.7	3.92	
	P-1	5.6	-	5.12 ~ 0.22		150	0.95	Residual
	D-17			1.24	2.70	22.8	4.45	
	91-Q	ri G		5.9	5.42	30.0	4.78	
	P-10	2,2	 	2.36	0.43	61.0	8/'#	
	P-9	2.0		8.68	9.70	w.7	9/1	
	R-3			31.4	90 19	4.	5.89	Steel Casing (rust)
	P-7	<u>.</u>		0.52	0.7	0.58	2.04	
	D-6	2.5		0. 4	0.07	0.0	20.7	
	+ - a			- 00 - 03 - 12	-0 -2	Ø	9,	
	P-2	4.5	and the second s	6.58	0,25	0.07	4.98	
	¥-8			9:24	00 00 00	0.45	0,60	
•	P-13	4.6		70.0	. w . w	0.02	67.0	
	R-5		•	50.6	1.07	0.38	2,69	steel Casing
							·	
.,.			•	•	- - -	-		
							•	
- : :								

	2	16
		1
	如果我们就是我们就是我们的人,我们就是我们的人,我们就是我们的人,我们就是我们的人,也是我们的人,我们也会会会会会会会会会会会会会会会会会会会会会会会会会会会会	NESE
		√NG/
教公室	The sale	W.S.
		.*
		25
		IE NT
		TACHIN

R-1 R-2 R-2A P-12 P-12 P-13 Coll D-17 D-17 D-17 D-16 D-17 D-16 D-17 D-17 D-18 D-19 D-19 D-10 D-11 D-12 D-13 D-14 D-15 D-16 D-17 D-18 D-19 D-19 D-10 D-11 D-12 D-13 D-14 D-15 D-16 D-17 D-18 D-19 D-19 D-10	PHASE Y PHASE XI REMARKS
0.73 0.73 0.73 0.73 0.73 0.11 0.14 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.01 0.01 0.01 0.01 0.02 0.01 0.01 0.01 0.02 0.01 0.01 0.01 0.02 0.01 0.01 0.01 0.01 0.01 0.02 0.01 0.02 0.01 0.02 0.01 0.02 0.01 0.02 0.02 0.01 0.02 0.02 0.03 0.01 0.02 0.03 0.01 0.02 0.02 0.03	h0.0
0.73 0.73 0.73 0.73 0.73 0.11 0.35 + 222 0.57 0.17 0.17 0.17 0.17 0.18 0.19 0.10 0.10 0.10 0.10 0.10 0.10 0.10	SI C.OI ERATED
0.73 0.73 0.73 0.73 0.11 0.12 0.14 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.10 0.02 0.02 0.04 0.04 0.05 0.05 0.05 0.05 0.07	0.03
0.73 0.73 0.73 0.73 0.11 0.11 0.10 0.10 0.10 0.10 0.10 0.25 0.25 0.25 0.42 0.42 0.42 0.42 0.03 0.00	90.0
0.73 0.73 0.11 0.14 0.20 0.42 0.42 0.42 0.42 0.42 0.03 0.00 0.00 0.02 0.03 0.03 0.04 0.04 0.05	i de la companya de l
0.73 0.11 0.10 0.10 0.20 0.20 0.42 0.42 0.42 0.40 0.00	-
0.14 0.10 0.20 0.20 0.40 0.40 0.027 0.04 0.027 0.04 0.027 0.04 0.027 0.04 0.027	
0.10 0.20 0.20 0.42 0.42 0.40 0.40 0.27 0.02 0.02 0.03 0.05	01.0
0.20 0.20 0.42 0.42 0.40 0.40 0.03 0.03 0.05	-
0.20 0.20 0.42 0.42 (0.40 (0.40 (0.03	<u>.</u>
0.20 0.42 0.42 0.40 (0.03 (0.01 0.03 0.27 0.27 0.14	
0.42 0.40 0.40 0.03 0.27 0.27 0.27 0.14	· · ·
7.03 7.03 7.03 7.05 7.05 7.05 7.05 7.05 7.07	
(0.1 0.05 0.27 1.02 0.27 0.14	<i>t</i> 1:0
1.3 0.27 1.02	
0.27	0.05
	· ·
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Boring	PHASE I	PHASE II	PHASE III	PHASE IX	PHASE X	Рнаве ХІ	REMARKS
R-i			1.>	0.05	1.0>	0.34	OI MG/L LETHAL
R-2			シ	0.1	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	<0.70	Ž
R-2A			0.15	0.08	40.1	4.10	TROUT & OVA
P- 12			0.18	0.05	<0.1	01.>	
H-d	0.05		.<.10		1,2	<u>0</u>	•
D-17		1	0.15	0.0 S	<0.1	\ \(\overline{0}\)	
91-Q	0.01	• .	01.>	<0.05	0	o/.v	
P-10	40.0		< 0.10	<0.05	<0·	01.	
P-9	50.0		0.0	20:02		ō.,	
R-3	•		0.26	<0.05	1.0>	0 V	**************************************
p-7	0.03		<0.10	<0.05	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	V-10	
P-6	G.02			<0.05	707	<.10	
P-4	0.03	·	0.22	<0.05	1.0>	٧. آن	
p-2	40.0		<0.10	<0.05	<0.1	0 6	
R-4		•	< 0.10	<0.05	7.0>	V.10	
P-13	0.04		0.13	0.05	<0.1	0/.>	
R-5	•		0,0	<0.05	<0.1	0.40	
•							
		1					
•	!			· · · · · · · · · · · · · · · · · · ·			

ATTACHMENT 27 BORING PHA R-1 R-2 R-2A	27 PHASE I						
	H BS:		COLIFORIN		MPN / 100 ML		
-2 2 A		PHASE II	PHASE 皿	PHASE IV	PHASE V	PHASE VI	REMARKS
2 2 A	·		230	79	2200	> 24000	Phase VI readings
2A			224,000	, ,	7	<i>8</i> 000	high overall - poss-
			2.2	42	740	80	dur
P- 12			> 16	#1	021	> 2400	day of sampling
P-11 9200	00	9200	> 16 ?	DRY	2 Z4000	> 24000	(110 mm / mm / mm)
D-17		29	23	2400	79	> 2400	
D-1.6 790	Q	760	7	^2	17	>2400	
P-10 1100	Q	[7	64	2	63	79	
P-9 22世	24000	1700	16000	230	9200	1660	
R-3			130	#	6.5	7600	
P-7	Q	2.2	13	K2	10	9.20	
330	50	2	v	2	< 2	> 2400	
4 230	0	3500	79	w w		920	
P-2 70		49	1	(3	90	7.9	
アーケ	1 1		27	23	700	>24000	
P-13 79	0	17	#6	9200	79	7.9	
R-5			\$	h	90	1600	
							STOOMPH / 100 ML 15

ATTACHMENT 28

FECAL COLIFORM - MPN 700 MI

																		e/i	
i i i i i i i i i i i i i i i i i i i		• ·	# · · · · · · · · · · · · · · · · · · ·				•	. ***								*.* * *			CRITERIA
>24000	u u	4		<u>.</u>	2 >		<2>	70	671	170	> 2400	2	< 2	1700	<i>N</i>	350			-
2.2	72	7	2	. 7	\ \ \ \	\ \ \	2 >		7 7	2>	75	7 7	25	<u>~</u>	7 7	7			
23				5 A A		•													
	< 2.2	j	<2.2	< 2.2		-	-				Beautiful and			1					
				'n	<2	2 >	\$	4.2		42	\$2	2 >	%		2	-			
												 				·			
R-1	R-2	R-2A	P-12	= -	D-17	D-16	P-10	P-q	R-3	p-7	P-6	p-4	P-2	R-4	P-13	R-5		:	
	33 22	33 22 <2.2 <2	33 22 \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	4 4 7 8 7 8	A	4	33 22 \langle 2.2 \rangle	33 22 \langle 2.2 \rangle	\$33 22 \$2.2	\$ \langle 2.2 \lan	Sample S	\$3	\$33	\$33 \\ \frac{2.2}{2.2} \\	42.2 33 22 42.2 DRY	\$2.2	\$2.2 \\ \langle 2.2 \	\$\frac{2.2}{\sigma_2}\$ \\ \frac{2.2}{\sigma_2}\$ \\ \frac{2.2}{\sigma_2}	\$ \\ \frac{\chi_{2.2}}{\chi_{2.2}} \\ \frac{\chi_{2.2}}{\chi_{2.2}

6.8 / 7.5 7.6 / 7.5 7.6 / 7.5 6.1 / 7.7 6.1 / 7.7 6.2 / 7.7 6.3 / 8.3 6.4 / 7.7 6.7 / 7.7 6.7 / 7.7 6.7 / 7.5 6.7 / 7.7 7.7 / 8.3 7.7 / 7.8 7.7 / 7.8	BORING	PHASE I	PHASE I PHASE II	PHASE III	PHASE IV	PHASE Y	PHASE XI	REMARKS
6.87.72 6.97.8.1 7.67.74 7.4 7.5 7.5 7.5 7.5 7.5 7.5 7.5 7.5 7.5 7.5	R-1			8.3 / 8.0	7.4	7.9	7.1	
6.77.7.2 6.97.8.1 7.67.7.4 7.4 7.9 7.5 6.97.8.1 7.67.7.8 7.8 7.8 7.8 7.8 7.8 7.8 7.8 7.8 7.	R-2			6.8/7.5	7.3		80	**************************************
6.7/7.2 6.9/8.1 7.6/7.6 7.6 7.5 7.5 7.5 7.5 7.8 7.8 7.8 7.8 7.8 7.8 7.8 7.8 7.8 7.1 7.2 7.1 7.2 7.1 7.2 7.1 7.2 7.1 7.2 7.1 7.2 7.1 7.2 7.1 7.2 7.1 7.2 7.1 7.2 7.1 7.2 7.1 7.2 7.1 7.2 7.1 7.2 7.1 7.2 7.1 7.2 7.2 7.1 7.2 7.2 7.2 7.1 7.4 7.0/8.0 6.6/7.5 7.2 7.2 7.2 7.2 7.2 7.2 7.1 7.1 7.2 7.1 7.2 7.1 7.1 7.2 7.1 7.1 7.1 7.2 7.6 7.1 7.1 7.1 7.2 7.6 7.1 7.1 7.1 7.2 7.6 7.1 7.1 7.1 7.1 7.2 7.6 7.1 7.1 7.1 7.1 7.2 7.6 7.6 7.1 7.1 7.1 7.1 7.2 7.6 7.1 7.1 7.1 7.1 7.1 7.1 7.1 7.1 7.1 7.1	R-2A		-	7.0/1.4	7.4	7.9	7,5	
6.777.2 6.97.8.1 7.677.8 7.8 7.8 7.8 6.877.3 6.877.8 6.477.7 7.2 7.1 7.2 7.1 7.2 7.1 7.2 7.1 7.2 7.1 7.2 7.1 7.2 7.1 7.2 7.1 7.17.4 7.07.8.1 6.17.7 7.5 7.3 7.3 7.4 7.477.8 7.2 8.0 6.67.7.5 7.7 7.6 7.8 7.8 7.17.4 7.07.8.0 6.67.7.5 7.7 7.4 7.4 7.17.8 7.17 7.4 7.4 7.17.8 7.17 7.4 7.4 8.1 7.4 7.17 7.17 7.18 8.0 6.77.7 7.18 8.0 7.6 7.18	P-12	3		7.6/7.6	7.6	7.5	7.3	
6.8/7.3 6.8/7.8 6.4/7.7 7.2 7.1 7.3/7.7 6.9/8.1 6.2/7.7 7.2 7.7 7.1/7.4 7.0/8.1 6.1/7.7 7.5 7.3 7.1/7.4 7.0/8.2 6.0/8.0 7.7 7.6 7.1/7.4 7.0/8.0 6.6/7.5 7.7 7.2/7.6 7.1/8.0 6.7/7.7 7.2 7.1/7.8 6.9/8.0 6.7/7.7 7.7 7.4 7.6 7.1/8.0 6.7/7.7 7.2 7.6	Ī	6.7/7.2	6.9 / 8.1	7.6/7.8		7.5	2.3	
6.8/7.3 68/7.8 6.4/7.7 7.2 7.1 7.3/7.7 6.9/8.1 6.2/7.7 7.5 7.7 7.7 7.5 7.3 7.7 7.6 7.8 7.8 7.1 7.6 7.8 7.8 7.1 7.6 7.8 7.1 7.6 7.1 7.6 7.1 7.6 7.1 7.6 7.1 7.6 7.1 7.6 7.1 7.1 7.1 7.1 7.1 7.1 7.1 7.1 7.1 7.1	D-17		7.5/8.1	7.3 / 8.3	7.8	7.8	7.6	· · · · · · · · · · · · · · · · · · ·
73/7.7 6.9/8.1 6.2/7.7 7.5 7.7 7.3 7.3 7.7 7.6 7.8 7.8 7.4 7.6/7.7 7.6 7.8 7.8 7.4 7.4/7.8 7.2/8.2 6.0/8.0 7.7 7.6 7.8 7.8 7.6 7.1/7.4 7.0/8.0 6.6/7.5 7.1 7.4 7.3 7.2 7.5 7.7 7.4 8.1 7.0/7.8 6.9/8.0 6.7/7.7 7.2 7.6 7.1/7.8 8.0 7.1/7.8 8.0 7.6	91-Q	6.8/7.3	68/7.8	1.7 / 1.9	7.2	7.1	7,9	
7.177.4 7.0/8.1 6.1/7.7 7.5 7.6/7.7 7.6 7.8 7.4/7.8 72/8.2 6.0/8.0 7.7 7.6 7.1/7.4 7.0/8.0 6.6/7.5 7.2 7.3 7.0/7.2 6.9/8.0 6.7/7.5 7.7 7.4 7.0/7.8 6.9/8.0 6.7/7.7 7.2 7.6 7.0/7.8 6.9/8.0 6.7/7.7 7.2 7.6	P-10	7.3/7.7	6.9/8.1	6.2/77	7.5	7.7	7.3	
7.4/7.8 7.2/8.2 6.0/8.0 7.7 7.6 7.1/7.4 7.0/8.0 6.6/7.5 7.6 7.3 7.0/7.2 6.9/8.0 5.9/8.3 7.2 7.4 7.2/7.6 7.1/8.0 6.7/7.5 7.7 7.4 7.0/7.8 6.9/8.0 6.7/7.7 7.2 7.6	P-9	42/12	70 / 8.1	27.77.9	7.57	7,	75%	
7.4/7.8 7.2/8.2 6.0/8.0 7.7 7.6 7.1/7.4 7.0/8.0 6.6/7.5 7.6 7.3 7.0/7.2 6.9/8.0 5.9/8.3 7.2 7.7 7.2/7.6 7.1/8.0 6.7/7.5 7.7 7.4 7.0/7.8 6.9/8.0 6.7/7.7 7.2 7.6 7.1/7.8 8.0 7.6	R-3				9,7	.00	7.	
7.1/7.4 7.0/8.0 6.6/7.5 7.6 7.3 7.0/7.2 6.9/8.0 5.9/8.3 7.2 7.3 7.2/7.6 7.1/8.0 6.7/7.5 7.7 7.4 7.0/7.8 6.9/8.0 6.7/7.7 7.2 7.6 7.1/7.8 8.0 7.6	P-7	7.4/7.8	7.2 / 8.2		7.7	7.6	, 1, 5 W	
7.0/7.2 6.9/8.0 5.9/8.3 7.2 7.3 7.2/7.6 7.1/8.0 6.7/7.5 7.7 7.4 7.0/7.8 6.9/8.0 6.7/7.7 7.2 7.6 7.1/7.8 8.0 7.6	p-6	7.1/74	70/8.0	1	9.7	7.	7. 2	
7.2./7.6 7.1/8.0 67/7.5 7.7 7.4 6.9/7.1 7.9 8.1 7.0/7.8 6.9/8.0 6.7/7.7 7.2 7.6 7.1/7.8 8.0 7.6	4- d	7.0/7.2	6.978.0	/	7.2	in in	2.0	
7.0/7.8 6.9/8.0 6.7/7.7 7.2 7.6 7.6 7.1/7.8 8.0 7.6	P-2	7.2./7.6	7.17/8.0	/	7.7	<i>†''</i>	72	
7.0/7.8 6.9/8.0 6.7/7.7 7.2 7.6 7.6 7.1/7.8 8.0 7.6	R-4			7/2	7.9	Qo	jo O	
7.1/7.8 8.0 7.6	P-13	7.0/7.8	6.9 / 8.0	1	7.2	7.6	7.7	
	5. 12			7.1/7.8	8.0	7.	7.6	
					•			

ATTACHMENT 30

CALCIUM LEVELS - MG/I

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\$	v	170																		
REMARKS	Σ	LICIA	のフィ			•												•		
œ	CALCIUM IS	BENEFICIAL	エしMALの													:				
-	Ú	а	 -	- · · · · · ·									:					·	- :	
PHASE VI	40.6	70.6	22.2	82.8	6.97	39.1	8.87	49.2	28.6	28,6	25.0	6.97	46.9	46.1	187.5	65,0	39.1		•	
N															<u>.</u>		.*	 : · · ·		
P-ASE X	319	9	80	0	48	7	53	n n	109	6 7	45	700	5	76.6	353	95	•			
ZI.	9	0	0	0		0	0	0	0											
PHASE IX	350	49.0	43.0	76.0		52.0	57.0	59.0	121.0	62.0	51.0	70	52.5	87.0	90	110	7.69		1	
Ħ		:										:			·	· . ;			ī	
PHASE III		,						_												
Ħ									:			1								
PHASE												:	٠			: ::				
H									7		·					·				
PHASE I		************			20		in O	9	127		47	73	U U	40		86				
U Z			∢	ત	-	_	·					:							:	
Boring	R-1	R-2	R-2A	4	Ġ.	0-17	D-14	P-10	6-0	Д 6	P-7	P=6	P-4	9-2	R-4	P-13	50 10			

ATTACHMENT 31

MAGNESIUM - MG/L

				1						:						. •		··	····	
REMARKS		• •				•										•			-	
REM						- ·	and and and and and and and and and and		•					- · · · · · · · · · · · · · · · · · · ·		-				
PHASE VI	113	34.7	26,6	46.8	31.5	29,1	14,0	ы 22 23	12,5	13.00	6://	,	60	20.6	680	30.3	13,8	•		
PHASE Y	906	7.4	. 82	50	80	80	80	w.	9	2	72	w 0,	<u>N</u>	8	: †	, t	9			
PHASE IV	0+01	m	29	53.5	•	30	ဝဗ္ဗ	m	2.4	1	Ñ	m in	70	5.0	00	43	29			
PHASE III				Jahrana Jaha Jahrana Jaha Jaha Jaha Jaha Jaha Jaha Jah Jaha Jaha Jaha Jah Jah	e e e e		· · · · · · · · · · · · · · · · · · ·			in a control of the c						•				
Phase II			-					:	-						-					
PHASE I					26		25	29	.50		7	2.9	ā	27		ି ମ ଫ				
Boring	- -	R-2	R-2A	P-12	P	D-17	91-Q	P-10	P-9	R-3	P-7	9-6	±-d	P-2	R-4	P-13	7. 13.			

ATTACHMENT 32 BICARBONATE LEVELS - 1

1								÷ ;			•			· ·	3	·			
			•					The second secon											
29	183	061	202	152	217	24.5	240	126	121	1.10	(3/	1/8	167	25	235	127			
611	242	761	243	219	216	991	226	346	190	235	229	(58	207	011	266	258			
601	187	061	462		612	160	6/2	414	2/4	220	220	38	208	108	268	234			
				237	249	να Φ	273	476		266	274	190	259		1				
		**************************************		185		- 80	270	425		250	285	061	270		305	•			-
R-1	۵. در	R-2A	P- 12	=	-17	91-Q	P-10	p-d	R-3	P-7	9-6	+-0	P-2	カーキ	P-13	R-5			
	611 601	109 119	511 601 611 601	109 119 187 242 190 194 234 243	109 119 187 242 190 194 234 243 185 237	109 119 187 242 190 194 234 243 219 216	185 237 237 242 190 194 237 234 243 249 219 219 180 185 160 166	165 237 185 237 237 242 185 237 249 219 249 219 270 273	165 237 185 237 185 237 237 234 249 219 249 219 270 273 270 273 270 273 270 273 270 273 270 273 270 273 270 273 270 274 270 273 270 274 270 275 270 276	169 119 185 237 185 237 237 234 249 219 270 273 270 273 270 273 270 273 270 273 270 273 270 273 270 273 270 273 214 414 396	169 119 187 242 187 242 180 194 219 219 249 219 270 273 270 273 270 273 270 273 219 226 250 226 250 235	169 119 185 237 242 186 237 249 180 185 219 219 270 273 219 226 425 476 414 396 425 246 220 235 285 220 229	185 237 242 185 237 242 190 194 219 243 249 219 219 270 273 219 226 476 166 270 273 219 226 414 396 425 475 416 425 416 190 250 266 220 235 219 220 235 219 220 235	109 119 119 119 119 119 119 119 194 242 190 194 243 249 219 216 166	109 119 119 119 119 119 119 119 119 119 119 119 119 119 119 119 110 119 110	109 119 119 119 119 119 119 119 119 194 242 190 194 243 219 219 219 219 226 190 190 190 190 138 158 158 270 259 220 229 220 229 235 250 259 207 208 207 208 205	169 119 119 119 119 119 119 119 119 194 242 242 243 249 249 219 219 219 219 229 226 220 225 220 225 220 225 220 225 220 225 220 225 220 225 220 225 220 225 220 225 220 225 220 225 220 225 220 225 220 225 226 226 226 226 226 226 225	165 237 234 242 185 237 249 216 180 185 273 219 216 1425 476 160 166 270 273 219 226 250 266 220 235 265 274 220 226 250 266 226 270 259 208 207 270 259 208 207 270 259 208 207 285 208 207 285 208 208 285 208 208 285 208 208	185 237 234 242 180 185 242 180 185 243 249 219 216 270 273 219 216 476 414 396 250 266 220 235 285 274 235 285 274 28 270 259 220 270 259 207 285 207 285 207 285 207 285 207 286 266 270 259 207 286 266 270 259 207

LTACHMENT 33

POTASSIUM - MG/L

PHASE II REMARKS	9	07)	0,7	20.2	2.0	Z:0	Jo.	9,4		0		, a	9	<i>S</i>	7	0.7	90,0		
PHASE X	260	 6.	1.7	8.	∞		_ '	7.		6	0,1	7	<u>v</u>	# #	- 6	0.7	2,3		-
PHASE IX	260	5.	ln O	. 2		7.0	la -	. 70	- 10	0	r)	, do	lo	lo	1300	n Q	0	-	
PHASE III		Alega,	· · · · · · · · · · · · · · · · · · ·			And the second s				and a ware special control of the co	and the second s						· ·		
PASE I		•		10 mg		Company of										• • • • • • • • • • • • • • • • • • • •			
PHASE I		- :						•		And the second s	2 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4							:	
BORING	R-1	R-2	R-2 A	P- 12	=	D-17	91-Q	P-10	P-9	R-3	P-7	P-6	p-4	P-2	₹-¥	P-13	10 10		

ATTACHMENT 34

FLUORIDE - MG/L

Boring	PHASE I	PHASE II	PHASE III	PHASE IV	PHASE Y	Рнаве 🎞	REMARKS
R-1		ŭ		6:0	1.1	0,3	* LEVEL BETWEEN
R-2		÷		9.	91.0	0.5	60 60 60 60 60 60 60 60 60 60 60 60 60 6
R-2A				9.	N O	0,2	
P- 12				0.7	0.7	6,2	
		0.1		DRY	9.0	9	
D-17		0.19		0.2	0.7	0.	-
91-0		0.16		0.	9	0.1	
P-10		0.21		0.2	0.5	o,	
P-9		0.22		0.7	o,	4.0	
R-3				0	0.2	n,	
P-7		09 0		90	9;0	ó	
9-d		0.22		o'	w.	en 0	
-d		0.76		0,2	, o	<i>i</i> 2	
p-2		0.20		0.7	i Q	o, W	
R-4				6.		6	
P-13	• • •	0.22		. N	o w	. o	*
7. 12	·			N	0,2	0.4	
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